September 7, 2016

# Geotechnical Soils Investigation Report

Parking Deck 200 K Street, NW Washington, DC



4545 42<sup>nd</sup> Street, NW Suite 307 Washington, DC 20016 (202) 375-7900•www.geocapeng.com



September 7, 2016

Mr. Mark Corneal Office of the Deputy Mayor for Planning and Economic Development (DMPED) 1350 Pennsylvania Ave, NW, Suite 317 Washington, DC 20004

#### Subject: Geotechnical Soils Investigation Report, Parking Deck, 200 K Street, NW, Washington, DC (GeoCapitol Project No. DC16024)

Dear Mr. Corneal:

GeoCapitol Engineering LLC (GeoCapitol) is pleased to present the following geotechnical soils investigation report prepared for Parking Deck, at 200 K Street, NW, Washington, DC.

We appreciate the opportunity to serve as your geotechnical consultant on this project. Please do not hesitate to contact me if you have any questions or want to meet to discuss the findings and recommendations contained in the report.

Sincerely,

#### **GEOCAPITOL ENGINEERING LLC**

Daniel F. Gradishar, PE President dgradishar@geocapeng.com



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Figure 1: Site Vicinity Map

Appendix A: Subsurface Investigation Appendix B: Soil Laboratory Test Results



## 1.0 Scope of Services

This geotechnical soils investigation report presents the results of the field investigation, soil laboratory testing, and engineering analysis of the geotechnical data. This report specifically addresses the following:

- An evaluation of subsurface conditions within the area of the proposed site development, including a seismic site classification and site-specific spectral response.
- Comments on subsurface rock near the structure footprint.
- Comments on utilizing existing foundations for support of the proposed structure addition.

Services not specifically identified in the contract for this project are not included in the scope of services.

## 2.0 Site Description and Proposed Construction

The site is located at 200 K Street, NW, Washington, DC and consists of an existing parking deck straddling the I-395 tunnel. A site vicinity map is presented as Figure 1 at the end of this report. The ground surface elevation at the site ranges from EL 44 to 50 feet. Based on RFQ dated April 22, 2016, the proposed construction consists of an addition to the top parking deck on the existing parking garage structure. We understand from the review of the existing as-built drawings provided by DDOT and Carmel Plaza Apartments that the parking garage structure was originally designed to have townhouses or other residential structures located where the existing parking deck is being utilized to park vehicles off of 2<sup>nd</sup> Street, NW.



Note: Aerial Photograph from Google Earth Imagery Dated 2016.

## 3.0 Subsurface Conditions

Subsurface conditions were investigated by drilling a total of two (2) test borings in the proposed site development area. Test boring logs and a boring location plan are presented in Appendix A of this report.

Previous geotechnical engineering soil test borings completed during the design of the I-395 tunnel were provided by DDOT and reviewed by us. The soil test borings were completed by Tippetts-Abbett-McCarthy-Stratton Engineers and Architects (TAMSEA) dated April 1974. Although a geotechnical engineering report was not discovered, the subsurface information from that study has been reviewed as a part of this project.



Pertinent previous test borings by TAMSEA are also included in Appendix A of this report. Test boring data by others is assumed to be complete and accurate. We do not assume any responsibility for the completeness and accuracy of data obtained from others without our supervision.

#### 3.1 Geology

The site is located within the Coastal Plain Physiographic Province of the District of Columbia. The Coastal Plain consists of a seaward thickening wedge of unconsolidated to semi-consolidated sedimentary deposits from the Cretaceous Geologic Period to the Holocene Geologic Epoch. These deposits represent marginal-marine to marine sediments consisting of interbedded sands and clays. The Coastal Plain is bordered to the east by the Atlantic Ocean and to the west by the Piedmont Physiographic Province. The dividing line between the Coastal Plain and the Piedmont is locally referred to as the "Fall Line". This name comes from the waterfalls that form as a result of the differential erosion that occurs as streams cross the Piedmont/Coastal Plain contact.

Specifically, according to local geologic maps, the site is mapped in the Q5 gravel, sand, silt, and clay deposits of the Quaternary geologic period underlain by the clay-dominated lithofacies of the Potomac Formation of the Cretaceous geologic period. The Potomac Group sediments are the oldest sedimentary deposits in the Washington, DC area. These soils are known to be highly over-consolidated as a result of the weight of a substantial thickness of overlying soils that have since been eroded away. As a result of over-consolidation, Potomac Group soils have been pre-loaded and are capable of supporting substantial loads. The Potomac Group clays are well documented with problems associated with slope instability and excessive shrink/swell characteristics.



Map excerpt provided courtesy of the USGS (Fleming, A.H., Drake, A.A., and McCartan, Lucy, 1994, Geologic map of the Washington West quadrangle, District of Columbia, Montgomery and Prince George's Counties, Maryland, and Arlington and Fairfax Counties, Virginia: U.S. Geological Survey)

### 3.2 Published Soils

A review of the DC soils map on the DC Atlas Plus website and the NRCS-USDA Web Soil Survey indicates the site is mapped within the urban land soils.

### 3.3 Stratification

The subsurface materials encountered have been stratified for purposes of our discussions herein. These stratum designations do not imply that the materials encountered are continuous across the site. Stratum designations have been established to characterize similar subsurface conditions based on material



gradations and parent geology. The generalized subsurface materials encountered in the test borings completed at the site have been assigned to the following strata:

Stratum A (Existing Fill)	generally soft to firm or loose, poorly graded gravel, well graded sand, and clayey sand, FILL, with various amounts of concrete, organics, and sand, dry to wet, brown, yellow, and gray
Stratum B1 (Potomac Group)	firm to stiff, LEAN CLAY (CL), with sand and micaceous, wet, gray
Stratum B2 (Potomac Group)	Loose to hard, clayey SAND (SM) and POORLY GRADED SAND (SM), moist, yellow, red, and gray

The two letter designations included in the strata descriptions presented above and on the test boring logs represent the Unified Soil Classification System (USCS) group symbol and group name for the samples based on laboratory testing per ASTM D-2487 and visual classifications per ASTM D-2488. It should be noted that visual classifications per ASTM D-2488 may not match classifications determined by laboratory testing per ASTM D-2487.

#### 3.4 Groundwater

Groundwater level observations were made in the field during drilling. Groundwater was encountered at a depth of about 40 feet below the existing ground surface, or EL 10 at B-2.

The groundwater observation presented herein is considered to be an indication of the groundwater level at the date and time indicated. Where more impervious clay soils are encountered, the amount of water seepage into the borings is limited, and it is generally not possible to establish the location of the groundwater table through short term water level observations. Accordingly, the groundwater information presented herein should be used with caution. Also, fluctuations in groundwater levels should be expected with seasons of the year, construction activity, and changes to surface grades, precipitation, or other similar factors.

### 3.5 Soil Laboratory Test Results

Selected soil samples obtained from the field investigation were tested for grain size distribution, Atterberg limits, and natural moisture contents. A summary of soil laboratory test results is presented below, and the results of natural moisture content tests are presented on the test boring logs in Appendix A.

Test						eve ults	Atterberg Limits			Natural
Boring No.	Depth (ft)	Sample Type	Stratum	Description of Soil Specimen	Percent Retained #4 Sieve	Percent Passing #200 Sieve	u	PL	PI	Moisture Content (%)
B-1	23.5-25	Split- spoon sample	A	WELL GRADED SAND with silt and gravel (SW-SM)	19.3	8.7	NP	NP	NP	6.8
B-2	5-6.5	Split- spoon sample	А	CLAYEY SAND (SC)	0.2	23.6	51	16	35	13.1
B-2	23.5-25	Split- spoon sample	B1	LEAN CLAY with sand (CL)	0	82.1	40	16	24	22.1



Test					Sie Res	eve ults			Atterberg Limits	
Boring No.	Depth (ft)	Sample Type	Stratum	Description of Soil Specimen	Percent Retained #4 Sieve	Percent Passing #200 Sieve	LL	PL	PI	Moisture Content (%)
B-2	53.5-55	Split- spoon sample	B2	CLAYEY SAND (SC)	0	21.9	36	20	16	26.9

Notes:

- 1. Soil tests are in accordance with applicable ASTM standards
- 2. Soil classification symbols are in accordance with Unified Soil Classification System
- 3. Visual identification of samples is in accordance with ASTM D-2488
- 4. Key to abbreviations: LL = liquid limit; PL = plastic limit; PI = plasticity index; NP = non-plastic; N/T = not tested

### 3.6 Seismic Site Classification

Based on the results of the subsurface investigation and our knowledge of local geologic conditions, the site soils have been assigned to a site class D per the International Building Code (IBC). It may be possible to improve the site classification from a "D" to a "C" with in-situ shear wave testing at the site. We can provide this additional service upon request.

## 4.0 Engineering Analysis

Recommendations regarding utilizing the existing foundations for the proposed added load are presented herein.

### 4.1 Rock Excavation

Rock was not encountered in the recent borings to depths of 65 feet below the existing ground surface. Based on the previous boring logs drilled in 1974, auger refusal was not encountered to depths of 100 feet below the existing ground surface. However, very stiff Potomac Group sands and clays were encountered as borings were extended deeper.

### 4.2 Adding Loads to the Existing Foundations

The structural engineer, McMullan and Associates anticipates that the additional loading will require an increase of the soil bearing capacity of between 5 to 11 percent. We have reviewed the as-built foundation drawings. Based on the original design drawings, the foundations were designed for residential townhouses or similar lightly loaded residential structures to be constructed where the existing top parking deck is currently utilized to park vehicles. The structural field investigation will verify the structural integrity of the parking garage structure and is submitted under separate cover.

Based on our soil investigation data and review of the original design drawings, we estimate that the foundations are bearing in the Potomac Group dense sands and stiff clays. Based on our initial analysis, we believe that the existing foundations are capable of supporting the additional loads from the proposed one-level of construction on the parking deck. If additional stories or levels are planned above the 2-story townhouses, additional analysis and possible field investigations will need to occur.

## 5.0 General Limitations

Recommendations contained in this report are based upon the data obtained from the relatively limited number of test borings. This report does not reflect conditions that may occur between the points investigated, or between sampling intervals in test borings. The nature and extent of variations between test borings and sampling intervals may not become evident until the course of construction. Therefore, it is essential that on-site observations of subgrade conditions be performed during the construction period



to determine if re-evaluation of the recommendations in this report must be made. It is critical to the successful completion of this project that GeoCapitol be retained during construction to observe the implementation of the recommendations provided herein.

This report has been prepared to aid in the evaluation of the site and to assist your office and the design professionals in the design of this project. It is intended for use with regard to the specific project as described herein. Changes in proposed construction, grading plans, structural loads, etc. should be brought to our attention so that we may determine any effect on the recommendations presented herein.

An allowance should be established for additional costs that may be required for foundation and earthwork construction as recommended in this report. Additional costs may be incurred for various reasons including wet fill materials, soft subgrade conditions, unexpected groundwater problems, rock excavation, etc.

This report should be made available to bidders prior to submitting their proposals to supply them with facts relative to the subsurface conditions revealed by our investigation and the results of analyses and studies that have been performed for this project. In addition, this report should be given to the successful contractor and subcontractors for their information only.

We recommend the project specifications contain the following statement: "A geotechnical soils investigation report has been prepared for this project by GeoCapitol Engineering LLC This report is for informational purposes only and should not be considered part of the contract documents. The opinions expressed in this report are those of the geotechnical engineer and represent their interpretation of the subsoil conditions, tests and results of analyses that they performed. Should the data contained in this report not be adequate for the contractor's purposes, the contractor may make their own investigations, tests and analyses prior to bidding."

This report was prepared in accordance with generally accepted geotechnical engineering practices. No warranties, expressed or implied, are made as to the professional services included in this report.

We appreciate the opportunity to be of service for this project. Please contact the undersigned if you require clarification of any aspect of this report.

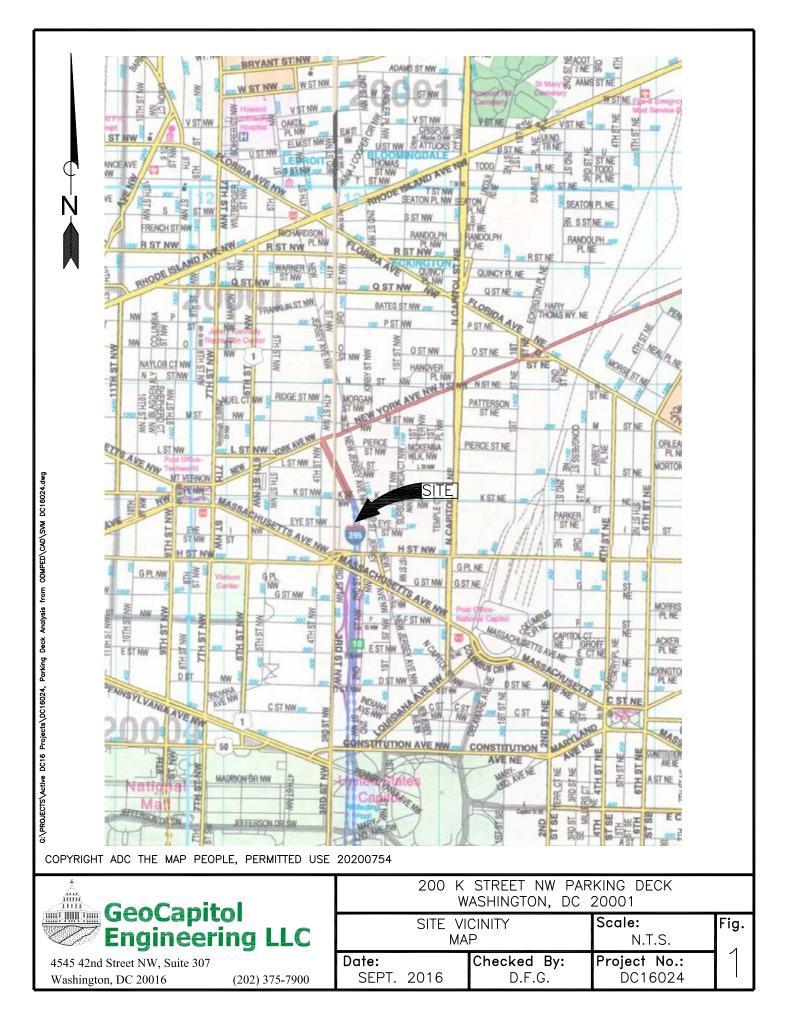
Sincerely,

#### **GEOCAPITOL ENGINEERING LLC**

Ashley Hogan, PG Senior Geologist Daniel F. Gradishar, PE Principal Copy: Ms. Polina Bakhteiarov (email

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## Appendix A Subsurface Investigation

Subsurface Investigation Procedures (1 page)

Identification of Soil (1 page)

Test Boring Notes (1 page)

Test Boring Logs (3 pages)

Previous Test Boring Logs (24 pages)

Boring Location Plan, Figure 2, (1 page)

Old Boring Location Plan, Figure 3 (1 page)



### Subsurface Investigation Procedures

#### 1. Test Borings – Hollow Stem Augers

The borings are advanced by turning an auger with a center opening of 2<sup>1</sup>/<sub>4</sub> inches. A plug device blocks off the center opening while augers are advanced. Cuttings are brought to the surface by the auger flights. Sampling is performed through the center opening in the hollow stem auger, by standard methods, after removal of the plug. Usually, no water is introduced into the boring using this procedure.

#### 2. Standard Penetration Tests

Standard penetration tests are performed by driving a 2 inch O.D., 1-3/8 inch I.D. sampling spoon with a 140-pound hammer falling 30 inches, according to ASTM D-1586. After an initial 6 inches penetration to assure the sampling spoon is in undisturbed material, the number of blows required to drive the sampler an additional 12 inches is generally taken as the N value. In the event 30 or more blows are required to drive the sampling spoon the initial 6 inch interval, the sampling spoon is driven to a total penetration resistance of 100 blows or 18 inches, whichever occurs first.

#### 3. Test Boring Stakeout

The test boring stakeout was provided by GeoCapitol personnel using available site plans. Ground surface elevations were estimated from topographic information contained on the site plan provided to us and should be considered approximate. If the risk related to using approximate boring locations and elevations is unacceptable, we recommend an as-drilled survey of boring locations and elevations be completed by a licensed surveyor.



### Identification of Soil

III.

I. DEFINITION OF	SOIL GROUP NAMES	ASTM D-2487	Symbol	Group Name
	Gravels	Clean Gravels	GW	WELL GRADED GRAVEL
Coarse-Grained Soils	More than 50% of coarse	Less than 5% fines	GP	POORLY GRADED GRAVEL
More than 50%	fraction	Gravels with Fines	GM	silty GRAVEL
retained	retained on No. 4 sieve	More than 12% fines	GC	clayey GRAVEL
on No. 200 sieve		Clean Sands	SW	WELL GRADED SAND
	Sands	Less than 5% fines	SP	POORLY GRADED SAND
	50% or more of coarse fraction passes No. 4 sieve	Sands with fines	SM	silty SAND
		More than 12% fines	SC	clayey SAND
		Inorganic	CL	LEAN CLAY
	Silts and Clays		ML	SILT
Fine-Grained Soils	Liquid Limit less than 50	Organic	OL	ORGANIC CLAY
50% or more passes the No. 200 sieve	50			ORGANIC SILT
the NO. 200 Sieve		Inorganic	СН	FAT CLAY
	Silts and Clays		МН	ELASTIC SILT
	Liquid Limit 50 or more	Organic	ОН	ORGANIC CLAY
				ORGANIC SILT
Highly Organic Soils	Primarily organic matter, dark	in color, and organic odor	PT	PEAT

#### **II. DEFINITION OF MINOR COMPONENT PROPORTIONS**

<u>Minor Component</u> Gravelly, Sandy (adjective) Sand, Gravel (with) Silt, Clay (with)	Approximate Percentage of Fraction by Weight 30% or more coarse grained 15% to 29% coarse grained 5% to 12% fine grained
GLOSSARY OF MISCELL	ANEOUS TERMS
SYMBOLS	Unified Soil Classification Symbols are shown above as group symbols. Use "A" Line Chart for
	laboratory identification. Dual symbols are used for borderline classification.
BOULDERS & COBBLES	Boulders are considered pieces of rock larger than 12 inches, while cobbles range from 3 to 12 inches.
WEATHERED ROCK	Residual rock material with a standard penetration test (SPT) resistance between 60 blows per foot.
ROCK/SPOON REFUSAL ROCK FRAGMENTS	Rock material with a standard penetration test (SPT) resistance of 50 blows for 1 inch.
RUCK FRAGMENTS	Angular pieces of rock which have separated from original vein or strata and are present in a soil matrix. Only used in residual soils.
QUARTZ	A hard silicate mineral often found in residual soils. Only used when describing residual soils.
CEMENTED SAND	Usually localized rock-like deposits within a soil stratum composed of sand grains cemented by calcium carbonate, iron oxide, or other minerals. Commonly encountered in Coastal Plain sediments, primarily
	in the Potomac Group sands (Kps).
MICACEOUS	A term used to describe soil that "glitters" or is shiny. Most commonly encountered in fine-grained soils.
ORGANIC MATERIALS	Topsoil - Surface soils that support plant life and contain organic matter.
(Excluding Peat)	Lignite - Hard, brittle decomposed organic matter with low fixed carbon content (a low grade of coal).
FILL	Man made deposit containing soil, rock, and other foreign matter.
CONTAINS	This is used when a fill deposit contains a secondary component that does not apply to a USCS
	classification. Only used for fill deposits
WITH	This is used when a residual soil contains a secondary component that does not contribute to its USCS classification. Only used for natural soils.
PROBABLE FILL	Soils which contain no visually detected foreign matter but which are suspect with regard to origin.
LAYERS	<sup>1</sup> / <sub>2</sub> to 12 inch seam of minor soil component.

COLOR

Two most predominant colors present should be described. Wet, moist, or dry to indicate visual appearance of specimen. MOISTURE CONDITIONS Fine-medium-coarse f-m-c



### **Test Boring Notes**

- 1. Classification of soil is by visual inspection and is in accordance with the Unified Soil Classification System.
- 2. Estimated groundwater levels are indicated on the logs. These are only estimates from available data and may vary with precipitation, porosity of soil, site topography, etc.
- 3. Sampling data presents standard penetrations for 6-inch intervals or as indicated with graphic representations adjacent to the sampling data.
- 4. The logs and related information depict subsurface conditions at the specific locations and at the particular time when drilled. Soil conditions at other locations may differ from conditions occurring at the test locations. Also, the passage of time may result in a change in the subsurface conditions at the test locations.
- 5. The stratification lines represent the approximate boundary between soil types as determined in the sampling operation. Some variation may be expected vertically between samples taken. The soil profile, groundwater level observations and penetration resistances presented on the logs have been made with reasonable care and accuracy and must be considered only an approximate representation of subsurface conditions to be encountered at the particular location.



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44.5 42.0				000	<i>Fill</i> , lig moist,	ht brown, POORLY GRA <b>GP</b>	DED GI	RAVEL, medium dense,	6+	4+13	14			
39.5				00	Very c	lense			19+	22+30	14			3.9
	5-			000	Dense	•			11+	13+22	12	•		
36.0	10 -			0	<i>Fill</i> , lig dense	ht brown, <b>f-c</b> , WELL GRA , moist, <b>SW-SM</b>	ADED S	AND with silt and gravel,	12+	19+23	19			
31.0	15 -		A		Very c	lense			12+	24+30	16		<b>&gt;</b>	
26.0	20 -				Dense				11+	22+20	18			_
	25-								12+	19+23	16	•		6.8
16.0 15.3	30 -	- - - -			Very c Auger	lense and Spoon Refusal at 29	).3 ft		12·	+50/3	12		>>	•
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THE STRATIFICATION LINES REPRESENT APPROXIMATE BOUNDARIES. THE TRANSITION MAY BE GRADUAL.

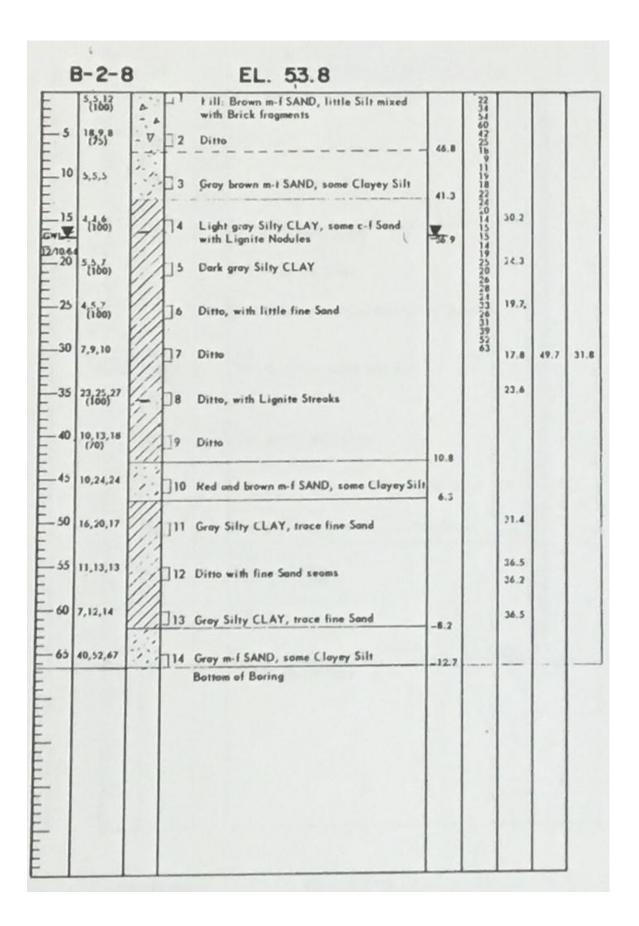


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	1	DC1	6024			50.0		Automatic hammer 2.2	5"						
ELEV. (ft)	DEPTH (ft)	SAMPLE TYPE	STRATUM	GRAPHIC		MATERIAL DES	CRIPT	ION			REC (in)	P TES	STAND ENETR ST RESI (BPI	ATION STANCE <sup>=</sup> )	MC (%)
50.0 49.5 47.5				00	<i>Fill</i> , lig	oil = 0.5ft. ght brown and yellow, POORL contains organics, medium d			13+	·11+9	14	/			
45.0	5-				-	ellow brown, <b>f-m</b> , clayey SANI Im dense	D, lo	ose, moist, <b>SC</b>		·4+4 +7+7	14 12	1			12.1
41.5									15		12	/			13.1
	10 -		A		Very lo	oose			0+	·0+0	10				_
36.5	15 -				<i>Fill</i> , lig contai	ght gray, POORLY GRADED ins concrete, loose, moist, <b>GF</b>	GRA ?	VEL with sand,	12-	+2+3	10	•			
31.5	20 -					<i>nac group</i> , gray, <b>f</b> , LEAN CLA vet, <b>CL</b>	Y wi	th sand, micaceous,	13-	+4+4	16				
	25 -								1+	2+3	12				22.1
21.5	30 -		B1		Stiff				5+	7+5	18				_
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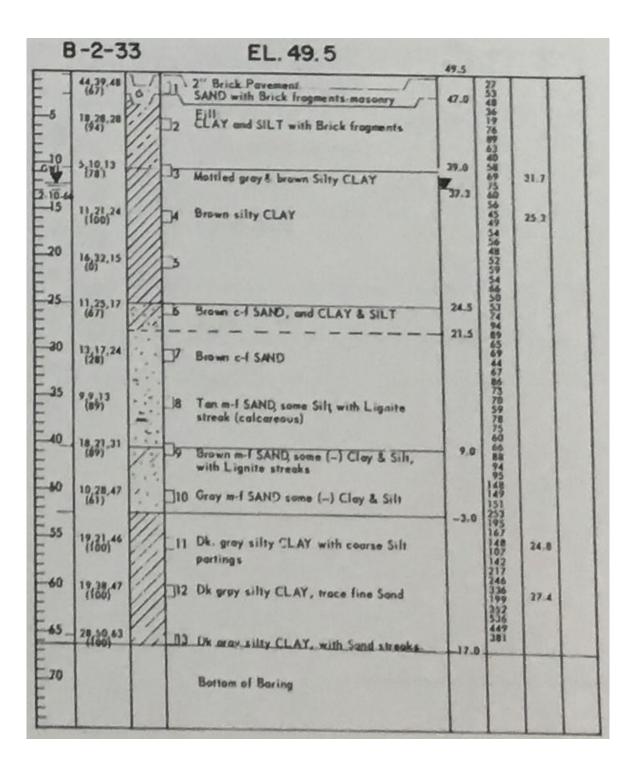
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					,, <b>.</b>	<b>,</b>			SOIL	
ELEV. (ft)	DEPTH (ft)	SAMPLE	STRATUM	GRAPHIC	MATERIAL DESC	RIPTION		REC (in)	PENETRATION TEST RESISTANCE (BPF)	MC (%)
		-			Potomac group, yellow and red, <b>f-m</b> , dense, moist, <b>SC</b> (continued)	, clayey SAND, medium				
	45 -		4				12+8+7	16		-
1.0	50 -		B2		Dark gray, wet		10+11+13	18	•	-
	55 -		>				4+7+11	18	<b>•</b>	26.9
-9.2	60 -		2		<i>Potomac group</i> , light gray, POORLY dense, moist, <b>SP</b>	GRADED SAND, medium	5+10+13	18		-
-13.5			,		Dense		15+21+28	16		
-15.0	65 -	$\square$			Bottom of Boring at 65.0 ft		13121120			
	70 -	-								
	70-	-								
	75 -	-								-
	80 -	-								-
GROUN	ND WAT						SAMPL	E TYPI	ES:	-
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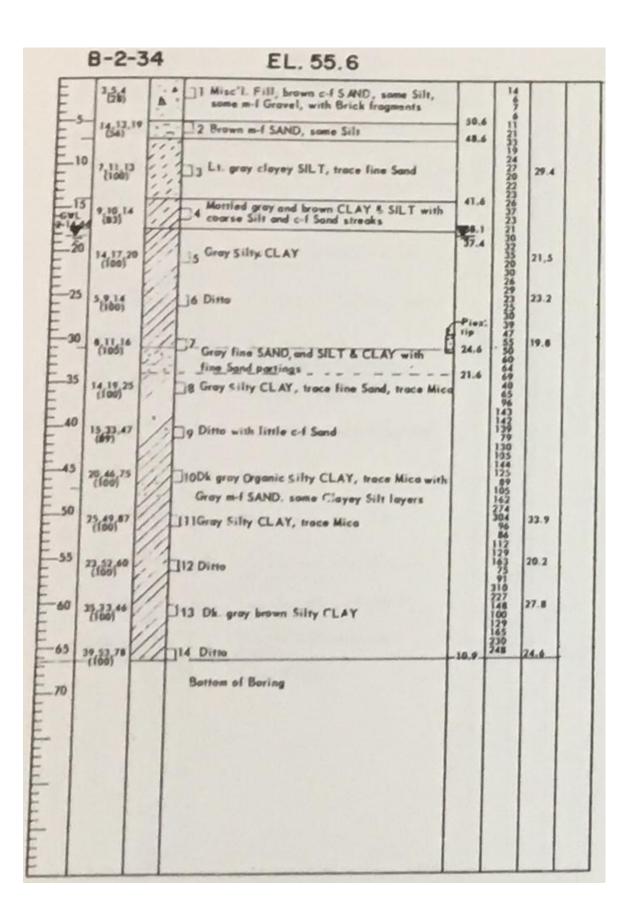
0 2,5,4 (80)	Fill: Red-brown CLAY & SILT and c-f SAND with Organic SILT streaks		78.5	27.5
-5 2,2,5 (100)	Fill: Red-brown CLAY& SILT, trace Sand	35.2	7 10 11 30	30.0
-10 9, 10, 12 (100)	3 Red brown fine SAND, some Silt	30.2	1011307338354743884	1.51
-15 7,7,9 (R0)	d Grey-brown Claysy SIL T, some fine Sand		41 36 30 41	19.7
20 3,4,3	Red-brown m-f SAND, some Clayey Silt with occasional 1/3" Organic Silt varves of low plasticity	20.7	50 36 31 34 34 34	24.4
25 173,200	6 - G CIGHT BROWN C-T SAMD, and C-I GRAYEL,	16.7 -15.7	200 - 2	
1/64 30 5,9,15	7 Dark grey Organic SilLT, medium plassicity with occasional fine Sand streaks		8888557787787757875492257925787549227 <b>X</b> 245555538388	41.8
15 à.7,11 (70)	a Grey c-f SAND		184248	
6,2,8	19 Light brown m-f SAND, little Silt	1.7	4751422	
7,6,7	10 Dark grey Organic SIL T, medium plo ticity mixed with some c-f Sand, trace fino Gravel	-5.3	393344	37.5
16,12,12 (70)	• •	-9.8	82.24	
5,4,5	712 Grey Silty CLAY and m-f SAND		51 54 47 53	23.6
6,7,9		18.8	81	25.8
100/5". 40/8". 6 4/6"	Grey m-f SAND, some Clayey Silt, trace fine Gravel Bottom of Boring	23.8	169 206 302	



B-2-31		EL.43.2	143.2	11
225°		Fill: Br. Silt and CLAY, little Sand mixed with brick fragments	*37.7	8 10 10 10 5
2 3317 -	1 32	Dise		
10 20,18,20		L.t. br. f SAND, lissle Sils, lissle stone frogments	+29.2	8 657 547 657 67 67 67 67 67 67 67 67 67 67 67 67 67
15 18,20,27 (26)	04	L1. gr. br. SILT and I Sand		44 40 42 54
20 20,60 (25) - 20,66,103 (67)		L.t. br. m-f SAND trace Silt Grbr. c-f SAND, little Silt, some m-f Gravel Ditto Dk. br. c-f SAND, little Silt, some m-f Gravel	+16.7	14 80 490 495 31 31
2 60	tillo	Dk. gr. Organic Silly CLAY		45 28.9 57 79
2 (35) 2 (35) 2 (35)	10	Grbr. m-I SAND, trace Silt with few 1/16" Silty Clay varves	-113	80 4700 4951 4577 4577 4577 4577 4577 4577 457 557 5
NL 15 25,37 25 (61)	: p.	Lt. gr. f SAND		2439422
40 20,26,39		Ditto	=0.2	68 63 78 87 87
45 2273,20	: : Jis	Gr. e-I SAND and m-I Gravel, trace Silt	-4.8	78 47 45 45 45
50 0.9,10	1/214	Gr. Silry CLAY, trace Sand with m-f Gravel pieces		62 104 135 82 82
55 0,13,20 (03)	1215	Gr. Siley CLAY, trace Sand		97 160 109 117 225
60 8,12,18 (100)	110	Ditts	-18.3	
69 (17).20	70			50 1 0 50 1 0 450
70 720180	1 Tu	Gr. m-I SAND, some Sili with pockets of gr. Silty CLAY, little Sand	28.3	
75		Bottom of Boring		
60				

+ 53.2 16 61 84	
39 18 34 34	
1245580	
12222	
2118 6 B	
75 70 49 87	
73 64 69 105	23.6
124	
142	
205	
168	
463	
146	26.3
7 168	
1	
	8498845564480321224518689509774952349328229

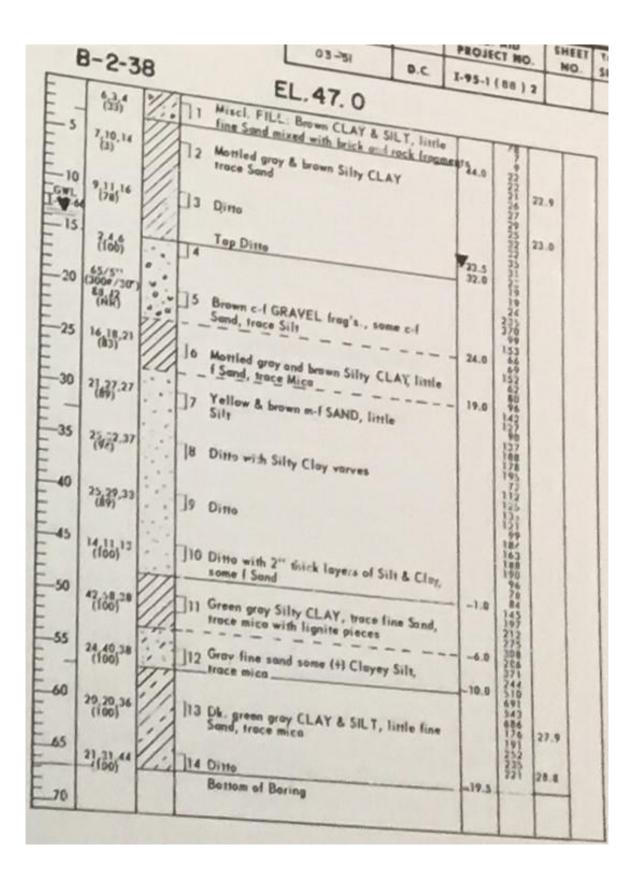


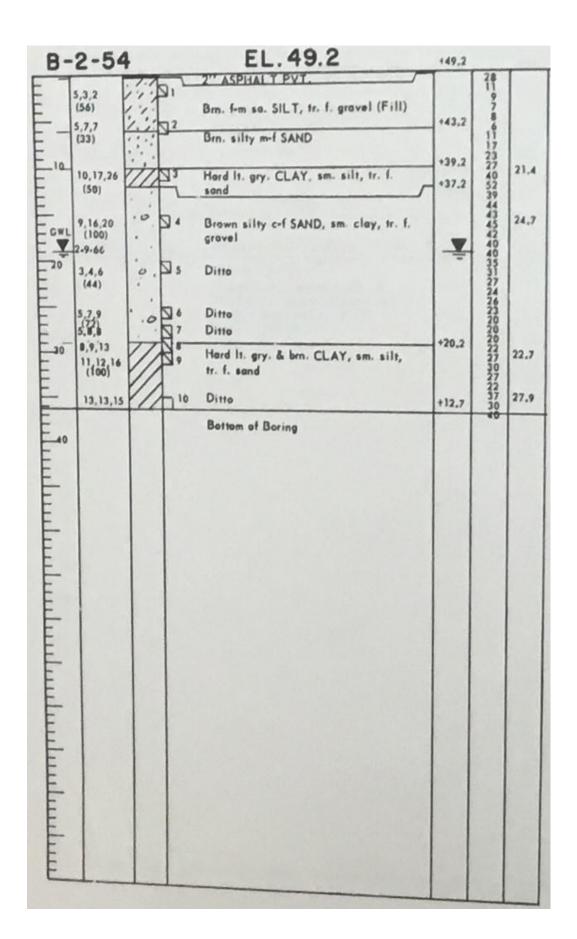


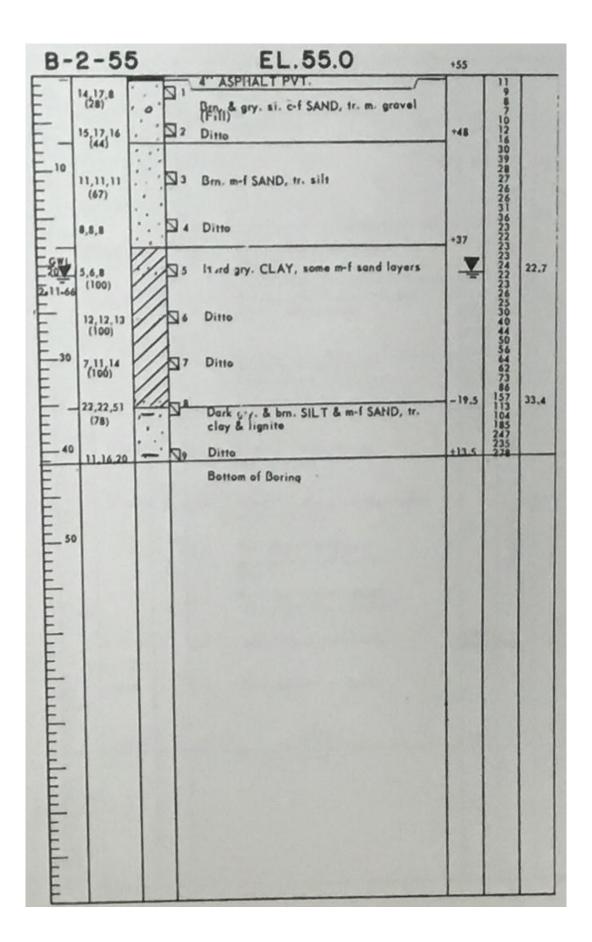
-35 30,1001 29,46,53 (100) 27,42,48 -35 27,42,48 -40 40,47,53 -40 40,47,53 -40 40,26,18 -50 29,94,105 -50 29,94,105	- 47.0 40.0 ••• ••• ••• ••• ••• ••• ••• ••• •••	38 434 357	23.3 20.7 23.3 25.9 28.7	
60 25,47,66 ,	-19,5-			

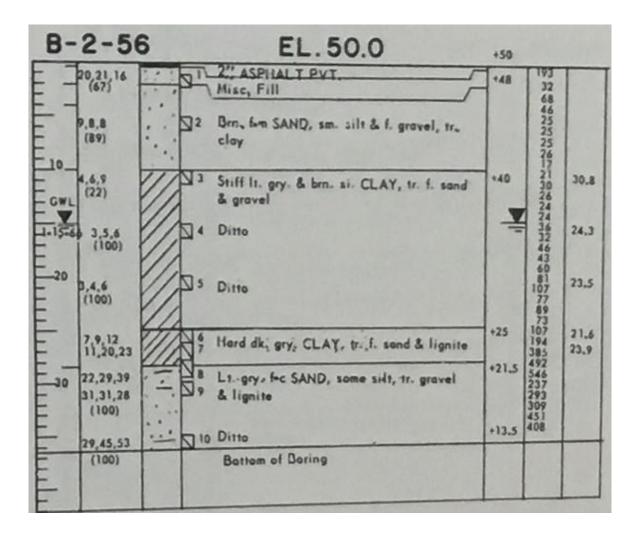
B	3-2-3	36		EL.45.2				
-	9,7,7 (60)	1.1	Ju	Mise'l. Fill, graybrown SILT and e-FSAND with Brick fragments	43.0	14		
5	8,18,28 (75) <sup>28</sup>		12	Mottled gray brown CLAY & SILT with Lignite streaks, trace Mice	37.6	12224		
10	9,9,18 (100)	1	13	Brown fine SAND and SILT & CLAY, frace Mice		1177202472622888		
15	117,29		14	Yallow brown c-1 SAND and SILT, little m-1 Gravel, trace Mica	31.5	INSALL		
20	7,8,10 (100)	1	15	Gray silty CLAY	26.0	312858274482	22.6	
25	17,18,26 (100)	44	16	Gray fine SAND and clayey SILT with Lignite streaks	21.0	125		
30	, 20, 32, 45	14	57	Gray fine SAND, some Silt	17.5	20114		
35	8,12,36 (100)	11	18	Dk gray silty CLAY	10.0	20124 867 567 75 53 48 647	30.7	
10	12,20,41 (100)		19	Ditto		46517 34	30.1	
15	12,22,28	//	110	Dk gray CLAY & SILT trace Sand, trace Mica with coarse Silt or fine Sand parting		58 405 108 70 54 174 1286 57 77 77 127 76 55 7 57 127 7 127 7 127 7 127 7 127 7 127 7 127 7 127 7 127 7 127 7 127 7 127 7 127 7 127 12	26.8	
0	12,31,48	1.	111	Dk blue bray CLAY & SILT, trace Sand, trace Mica		64 174 286 85	21.9	
5	12,25,50	(1)	112	Ditto		77 127 163 85	27.7	
0	12, 39, 53	1.1	- 	Gray m.I SAND, some () clayey Sils,	14.0	57 65 96 184		
5				trace Mica Gray m-f SAND, little (-) Silt		109 77 78 117 181		
+	31,49,98		114	Sottom of Boring		-		
0								

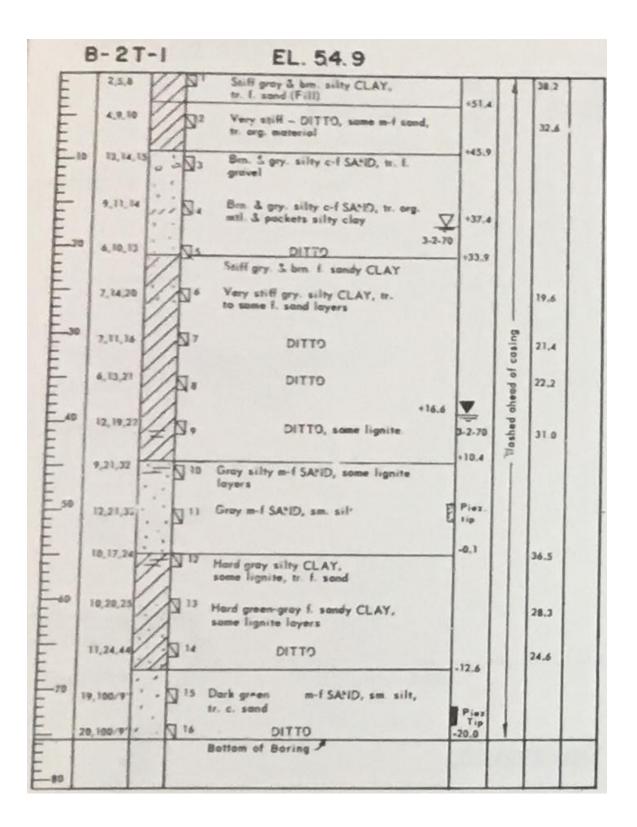
FO	B-2-	EL ACO THIS	1" DRAWIN	-	r
	6.8.6 (100)	Top: Miss Bill Com	OF THE	GRIGIN	BEEN REDUCE
Line	6,15,20 (100) <sup>20</sup>	Bot : Mostled gray and brown CLAY & SILT, medium plasticity	+44.0	27 9 10	
10	8,14,8 (56)	Dillo Dillo		10808050759008	20.6
C'NL	6,7,1) (100) 6	4 Brown CLAY & SILT with 15" fine Sand	-		24.1
20	109/4** (100) 9.12.13 (78)	a 15 Brown c-I SAND, come Gravel (wash)	+28.0	117789799	
30	9,14,16 (44) 7,8,20 (33)	7 Ditto with Lignite streaks 8 Ditto	+24.0	116 57 08	31.1
	29,37,56	9 Tan c-f SAND, some Clayey Silt	+18.5	127	34.5
40	33,44,36 (55)	10 Yellow white m-f SAND, some (-) Clayey		145570	
45	17, 16, 32 (22)	11 Cino		127 180 427 14557 1064 199 14557 1064 199 199 199 195552 109 109 109 109 109 109 109 109 109 109	
-50	12, 17, 57	12 Ditto with little Sile		179 185	
i	0,35,44 33)	- 13 Yellow brown m-f SAND, some Silt,		325	
	7,40,60	14 Blue gray fine SAND and (-) clayey SILT, trace Mica	-0.0	98 1187 184 432 434 242	
	0.32,54	115 Dinto		176 365 671	
65 (1	6,20,45	16 Gray fine SAND, some (-) Silt, trace Mica	-70.5	244 175 180 177	
70		Bottom of Boring			



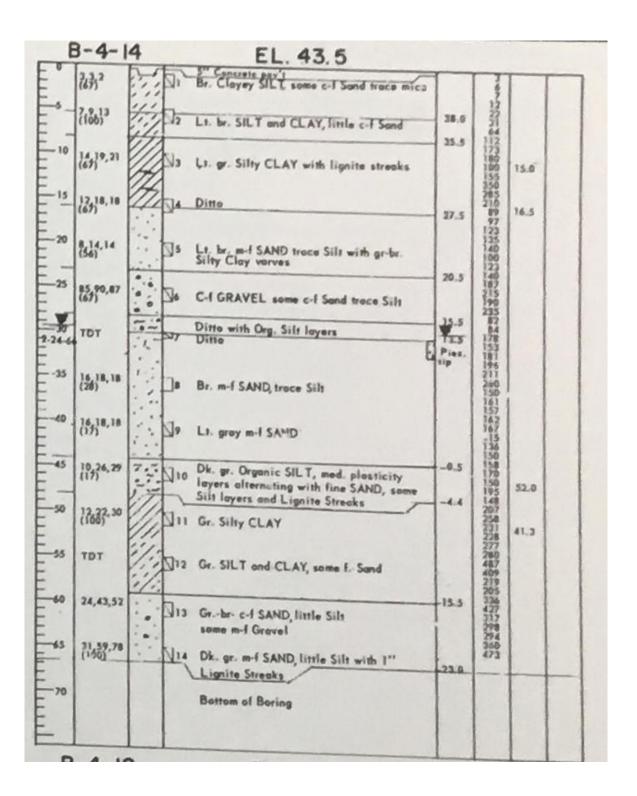








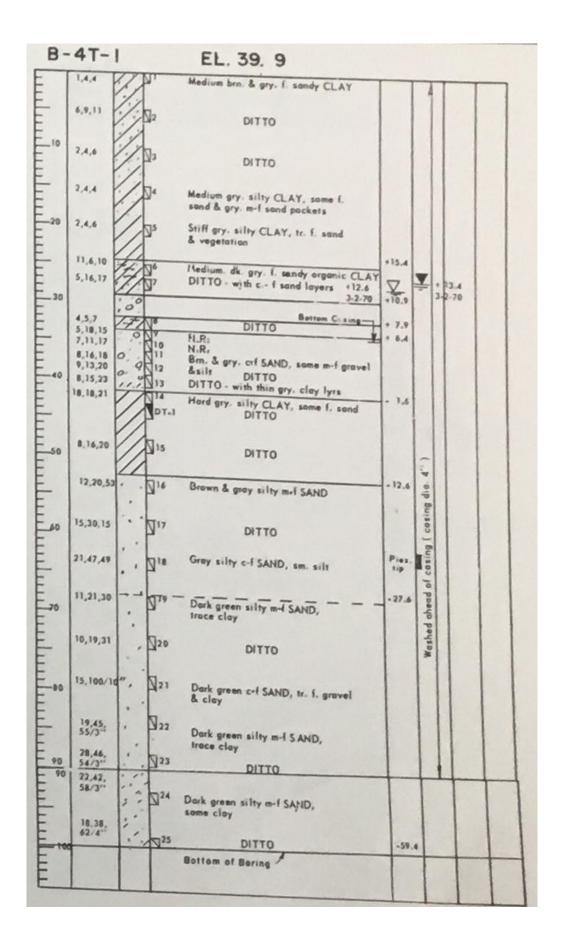
-2.T	-2	EL. 54.8			
7,17,22	°°.	91 Fill: Drn. c-f GRAVEL with some sond	+51.8		
7,6,6		2 Light gry & brn. c-f SA*ID, some some silt, tr. clay			
8,7,6	1.5			97495	
6,5,8	#	24 Stiff gry & brn. CLAY, tr. f. sond & lignite		7 8 10	23,8
3,5,7		5 Stiff gry. CLAY, tr. f. wad		21 19	20,2
4,6,1,1				20 27 31 31 39	20.0
9,14,23		07 DITTO	.21 5	65	19,3
28,52,83		some black lignite +16.4	GWL	115 180 143 190	
19,39,82		9 Gry, silty m-t SAND, tr. clay & lignite	3-2-70	147 165 194	
24,57,108	1.1			175+ 104 210 223	
26,36,38	1.1.	Il Gry. silty c-f SAND, tr. silt & clay nodules	+1.8	144 135 170 131	
13,18,32	1.1	12 Gry. silty f. SAMD, tr. clay		81 103 94 122	25.5
23,67,71		Bott: Mard gry-green SI. CLAT,	-6.2	209 182 180 199	20.5 24.9
28,83,165	11.	14 Green-gry, silty c-f SAND	\$11,7		
		GWL observed in cased borehole.			
		Date Depth of GWL - ft.			
		1-27-70 43'8"			
		2-16-70 38'8"			
		2-24-70 38'3'' 3-2-70 38'3''			
	2,17,22 7,6,6 8,7,6 6,5,8 3,5,7 4,6,1,1 9,14,23 28,52,83 19,39,82 24,57,108 26,36,38 13,18,32 23,67,71	7,4,6       8,7,6       6,3,8       3,5,7       4,6,1,1       9,14,23       28,52,83       19,39,82       24,57,108       13,18,32       13,18,32       14,23	7, 17, 22       ***       S1       Fill: Drn. c-f GRAVEL with some sond         7, 4, 6       S2       Light gry 3. brn. c-f SAND, some some some sill, tr. clay         8, 7, 6       S3       Light gry 3. brn. claysy c-f SAND         8, 7, 6       S1       Dick LIGNITE         6, 3, 8       Stiff gry 3. brn. cLAY, tr. f.       some 3. lignite         3, 5, 7       S       Stiff gry. CLAY, tr. f. so and         4, 6, 10       S6       DITTO         9, 14, 23       S7       DITTO         28, 32, 83       S       S         9       Gry. silty m-f SAND, tr.       e16.4         19, 39, 82       S       S         9       Gry. silty m-f SAND, tr.       e11.3         24, 57, 108       S       S         10       DITTO       e11.3         26, 36, 33       S       S         11       Gry. silty c-f SAND, tr.       e11.3         23, 67, 71       S       S         S	7,17,22       0       11       Fill: Drn. c-f GRAVEL with some sond       451.8         7,4,6       12       Light gry 3. brn. c-f SAND, some some silt, tr. clay       451.8         8,7,6       13       Light gry 3. brn. claysy c-f SAND       42.8         6,3,8       Stiff gry 3. brn. claysy c-f SAND       42.8         6,3,8       Stiff gry 3. brn. claysy c-f SAND       41.3         6,3,8       Stiff gry 3. brn. claysy c-f SAND       41.3         6,3,8       Stiff gry 3. brn. claysy c-f SAND       41.3         9,14,23       J7       DITTO         9,14,23       J7       DITTO         9,14,23       J7       DITTO         9,14,23       J9       Gry. silty m-f SAND, tr. clays fignite         19,39,82       10       DITTO         24,37,188       J11       Gry. silty m-f SAND, tr. clay silt 3. clay nodules         13,18,32       J12 Gry. silty c-f SAND, tr. clay       41.8         13,18,32       J13       Top: DITTO         23,67,71       J13       Top: DITTO         24,67,71       Light of Boring       GWL observed in cosed borehole.         Date       Dopth of GWL - ft. 1.1.7         Bottom of Boring       GWL observed in cosed borehole.         D	2,17,22       0       1       Fill: Dm. c-f GRAVEL with some some sond       151.8         7,4,6       12       Light gry 3, bm. c-f SAND, some some silt, tr. clay       151.8       142.8         8,7,6       13       Light gry 3, bm. clayey c-f SAND       142.8       15         8,7,6       13       Light gry 3, bm. clayey c-f SAND       142.8       15         8,7,6       13       Light gry 3, bm. clayey c-f SAND       142.8       15         8,7,6       14       Stiff gry 3, bm. clayey c-f SAND       142.8       15         9,14,23       14       Stiff gry. cLAY, tr. f. sand       16       170         9,14,23       16       Ditto       121.5       16         19,39,82       10       Ditto       10.4       10.4         19,39,82       10       Ditto       10.4       10.4         19,39,82       10       Ditto       10.4       10.4         19,39,82       10       Ditto       10.7       10.4         19,39,82       10       Ditto       10.4       10.4         19,39,82       10       Ditto       10.4       10.4         19,39,82       10       Ditto       10.4       10.4



B-4-15	EL. 52.4	52.4	
17,23,18	1 Misc'l. Fill, brown c-f SANC, some little m-f Gravel with Ashes	Site,	18228
	2 Brown c-I SAND, some Clayey Silt		32 28 21 43 89 56 42 47 42 21.1 109 216
		42.6	56 427
- 10 8 10 19	3 Gray Silty CLAY		42 21.1 109 216
15 5165	4 Ditto	35.9	255 291 19.6 147 125 110 20.1
CAL (98)	5 Dirto		110 20.1
-29 1186	5 Ditta high (+)		109 166 175 174
-25 74019 - 17	Ditto with Lignite streaks and Silt packets		106 159 166 175 174 180 201 18.7 207 255 253 253 203 21.0 294 186 596
30 (47)			235 253 203 21.0
30			715
35 24 49,131	Gray m-I SAND, little Silt, with few Lignite streaks		575 250 296 127 135
47 29, 38, 150 J10	Dinto		127 192 116 120
45 36,109,163	Green aray Sility CLAY	6.4	161 121 90 30.8 95 72 43 27.3
19 19 79 50 D12	Redish green Silty CLAY		38 13 67 75
55 25.54.116	Ditto	5	
50 70,49,97 (14 (160) 15	Ditto Blue gray fine SAND, some Silt	-10.6	00 60 83 24.9
15 70, 34,150 7 - 7.16	ilue gray f SAND, some cloyey Silt, m-f Sand pockets, few Lignite streaks	with	
	Bottom of Soring		

3-4-16	EL. 45.9	+45.9	
1418 11/1	Mottied gray and brown CLAY & SILT, medium (+) plast. with pockets of Silt		23 49 60
7,10,19	Top Ditto	+40.4	69 87 29 65 24.2
	Mattled gray and brown silty CLAY	-	79 81 119 59 28.2 101 102 143
s,20,37	Top Ditto Gray-brown c-f SAND, little Silt, some	429.9	126 89 394 344
17,46,53, (28) 19,75,65 (100) 7	c-f Gravel with silty Clay varves Lt. gray silty CLAY, tr. Sand with Lignite streaks and c-f Sand, some Silt layers Lt. gray m-f SAND, little Silt w. Lignite streaks Ditto no Lignite	+25.9	262 371 23.8 123 115 167 90 306 352
27,90,137	Top Ditto with wany Lignite_streaks	+15.9	477 576 722 109 196 152
20,52,94	Tan calcareous := { SAND, little Silt with silty Clay pockets		105 115 214 205
20,29,37 . 10	Ten silty CLAY	+4.9	90 95 120 176
27,68,181 /// VII	Ton calcareous m-f SAND, little Cloyey Silt		251 93 119 178 192 227
15 37 109 (100) T.D.T	Blue gray silty CLAY, little Sana Gray line SAND and SILT, trace Mice, with many 1/32" silty Clay streeks	-5.1	227 120 139 127 194 240 125
28,80,157	Gray SILT, some rule Sand, trace mice, with fine Sand, some Silt pockets Gray brown medium to fine SAND, trace	-12.1	270 315 383 397
47,104,170 (100)	(~) Silt		149 215 296 327 350
5 35.69.98 \$6 (100)	Grey I. SAND, and (-) SILT, trace Mica	-20.6	
	Bottom of Boring		

E	-4-1	7		EL. 45.6	45.6			
E .	(78) <sup>4</sup>		1	Brown c-f SAND, some (i) Silt, some (-) c-f Gravel	42.5	157487		]
5	8,12,24 (100)		2	Mattlej gray & brown silty CLAY		37 409 57 38	17.6	
2-21-64	9.13.12 (100)		33	Ditto	-36.3	98 160 95 105	28.8	
LIB-	12,14,10 (67)	14	S 4-	Brown c-f SAND, some clayey Silt, some m-f Gravel	30.0	111 100 262 287		
20-	14,15,19 (56)	11	25	Dk. gray Organic Silty CLAY, trace Mica	24.5	185 171 250 315 457		
E_25	12,17,17	11	36	Gray SILT & CLAY, some fine Sand		487 490 323 461	23.7	
113	TDT 24,40,56 (100)	11	7	Gray silty CLAY Ditta Lt. gray m-f SA'10, some (-) Clayey Silt	Plaz, tip 15.0	258 254 312 94 125 180		
35	12,39,111 (100) 1 D T	1	9	with some organic streaks Gray SILT & CLAY, trace fine Sand with coarse Silt partings Gray clayey SILT w. manyc. Silt partings	8.5	196 257 385 265 289	29.8 27.3	
E_40	27,35,61 (100)	111	Su	Gray clayey SILT, some 1. Sand, trace Mic	3.0	587 183 221 265 530	26.2	
45	29,68,125 (100)	11.1	J12	Gray m-f SAND, some (-) clayey Silt		520 1100 288 361 492 500		
50	37,28,190 (100)	1.	213	Gray m-1 SAND, some (+) Silt and Clay		388 370 451 1075		
55_	<0,55,100 (100)	1	14	Gray m-f SAND, little (+) clayey Silt	-9.5	382 336 851 1000+ 1000+		
60	30, 39, 100 (100)		215	Gray SILT, some line Sand, trace Mica			26.1	
-65	27,35,67		716	Gray fine SAND and clayey SIL T, trace Mica	-21.0		22.9	
70				Bottom of Boring				
75								
- 30								
					-	-	-tt-	-



F	1,5,19	Fill: Brn. & sandy clay, c. sand & gravel	.46.	1 18	
the state	4,3,3	D2 Mad. brn. zilty CLAY, some f. sond, tr. gravel		1 182 12 9 12 12 12 12 12	
10	1,1,2	DITTO 847-24 3-2-70		11 12 11 15 16	
1111	9,8,10	- DA Drown silty m-I SAND		35 42 36 44	
20	7,10,11	DITTO, with stiff brn. f. sondy clay 3 black streaks	+ 26.	70 43 41 1 35	25.3
	10,14,2	V/P		38 51 87 95 100 88	
- 30	5,18,21	The Very stiff gry. CLAY with lignite, Ir. 1 sone, Gray silty m-1 SAND 847-2 3-2-70	¥.	454 119 114 195 280 300	32.5
-	23,41,45	· · · · · · · · · · · · · · · · · · ·	Apz.	300 214 436 296	
- 40	25,30,42	<ul> <li>D &amp; Ditto, tr. c-f sa. streaks</li> <li>&amp; gry. clay nodules</li> </ul>	+ 4.1	320 378 143 300 330	
-	7,10,16	105tilf gry. silty CLAY with gry. m-f sand layers	- 0.9	300 240 75 106	39.5
- 50	23,46,79	N TI Geny silty CH SAND		252 360 754	
- 2	8,40,59	12 Ditto, with stiff gray clay layers	Pinz	600 685 531 220 410	
. 60	12,28,54	B47-2	tip	510	
	14,23,53			ahead	
70	12, 16,29	15 Grean-gry. hard silty f. CAND, with hard silty clay lyrs.		Washed ahead	
10	,18,3D	16 Dark green silty m-f SAND, tr. black clay		154 200 196 163 260	
80 1	3,22,39	17 Dark green silty m-I SAND		260 179 315 700 600 600	
10)	7,101,8	DIS DITTO		1	
0 3.	14.29	. Dis Dark green silty m-I SAFID			
	1.			Washed	
12,	21,41 /1	220 DITTO, with stiff sandy 5 clay layers & lignise Bottom of Boring	0.9		-

B-4T-3	EL. 48.2			
E 3,12,6	1 Misc. Fill Stiff brown silty CLAY, tr. f. sand	46.7	17	19.7
2,11,10		-+44.2	14 22 14 27 32 48 50 469 43 42 43 42 54 74	20.5
E 10 8,11,17			32 48 50 46	23,5
4.7.10	DITTO	Z +35.0 = 0.2-70 +31.2	49 43 42 54	
20 49,58,59 0. 1 15	Brown sandy m-f GRAVEL, tr. silt	E Piez.	74	28.0
- 49,39,39 - 1 . 1 . 1 3	Bottom of Boring	+26.7		
30	Piezameter installed at 20° - 4'' depth and sealed with bentonite at 10°. Water level at 13' 4'' depth on 2-5-70.			
50				
-60				
-				
-				

L

B-4T-4 B-4T-5)		EL. 48.2			
6,7,8	1/1	Fill: Brn. clayey sand	+45.7	16	19.8
6,13,17	22	Stiff brn. f. sondy CLAY, some silt B4T 5		16 15 16 22 32 51 46	
10 2,6,13	P		+37.7	46 31 39 44 47	25.0
3,5,7	30	DITTO	+30.7	30 48	25.7
20 57,143,12	18 22	Brown sandy m-f GRAVEL (angular), tr. silt			
4,8,12	FD.	Med. gry- silty CLAY, tr. f. sand & black lignite layers	+24.7 	47 5	25.2
13,27,47		Gry silty m-f SAND with occasional thin clay layers	+16.7	AT 5	
17,34,39		Red-brn m-f SAMD, sm. silt, tr. gravel with stiff f. sa. clay layer	Piez.		20,3
11,32,39		Red. brn. c-f SAND, sm. silt, tr. gravel	UHAT 4		
50 12,21,23		Black, brn. & gray silty c-f SAND tr. thin clay lyrs.		Washed ahead of casing	
10,25,41		Brn. silty c=f SAtID with green-gray f. sand lyrs. tr. clay		Washed	
60 8,17,50	- 12	Green-gry. silty m-f SAND, some clay & f. sand pockets			
32,74,154	. 213	Green-gray silty c-f SAMD	Piez Lip (B	4T 51	
3,8,24	. 1914	Dk. green silty m-f SAND			
9,19,36	115	DITTO	-26.8		
80		Bottom of Boring			

